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Nano Glass-Ceramic Lithium-Ion Conductive Buffer Layers for High Li-Ion Transport at Electrode/Electrolyte Interface for All-Solid-State Batteries

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Nano glass-ceramic lithium-ion conductive buffer layers with controlled composition and crystallization were prepared to generate stable Li-ion transport at the Lilsolid electrolyte interface under high current densities. In particular,  $Li_2O-B_2O_3$  glass was used as a sintering additive and interfacial buffer layer to modify the microstructure of  $Li_{6.5}La_{3}Zr_{1.5}Ta_{0.5}O_{12}$ (LLZT) and enhance the LilLLZT interfacial resistance. The effect of the  $Li_2O-B_2O_3$  addition as sol on the sintering behaviour of LLZT was investigated and compared with those using  $Li_2O-B_2O_3$  as powder. The ionic conductivity of the LLZT sintered with addition of  $Li_2O$ - $\rm B_2O_3$  sol and  $\rm Li_2O\text{-}B_2O_3$  powder achieves  $8\times10^{-4} \rm S$  cm $^{-1}$  (94%) and  $6.3\times10^{-5} \rm S$  cm $^{-1}$ ( 78 %) at room temperature, respectively. Moreover, Li|LLZT interfacial resistance became lower than those without the use of  $Li<sub>3</sub> BO<sub>3</sub>$ , achieving a critical current density of 10 mA cm−<sup>2</sup> . The results suggest that the interfacial inorganic layer can favour not only the sintering of solid oxide-type electrolytes but also the interfacial electrode/electrolyte resistances.

#### **1.Introduction**

All-solid-state batteries are one of the most promising candidates for energy storage systems with high energy density. Nowadays, several solid electrolytes with exceptional high ionic conductivities and wide electrochemical windows have been obtained, making them not only compatible with high-potential electrodes but also a safe alternative for energy storage. Although the advantages of the solid electrolytes, the realization of all-solid-state batteries still remains elusive mainly due to high electrode/electrolyte interface resistance. All-solidstate batteries based on oxide-type solid electrolytes  $(L_{6.5}L_{3.2}Zr_{1.5}Ta_{0.5}O_{12}$ , LLZT) are of particular interest because of chemical compatibility with lithium metal as anode. In this regard, the main challenge is to reduce the interfacial Li/solid electrolyte resistance and prevent the dendrite formation at high current densities.

Li alloys  $[1,2]$  are one of the most used strategies to reduce the interfacial resistance between LLZ  $(L_i \text{L}_3 Zr_2 \text{O}_{12})$  solid electrolyte and lithium metal (LilLLZ interface). Our group<sup>[3]</sup> have proposed the use of an amorphous  $Li_2O-SiO_2$  buffer coating. These strategies significantly reduce the LilLLZ interfacial resistance. However, the current limit density, at which the cell is shorted by lithium dendrite formation, is still low and far from the current density required for the fast-charge goal (10 mA cm<sup>-2</sup>)<sup>[4]</sup>. Ideally, new alternatives to handle free-dendrites Lilsolid electrolyte interface at high current density should have adequate Li-ion conductivity allowing for the stable distribution of the high current densities and maintaining the integrity of the solid-solid contacts. In this sense, the lithium alloys seem impractical as the large volume changes<sup>[5]</sup> (e.g.  $100-400\%$  for Li–Si and Li–Al alloys) could certainly threaten the integrity of solid-solid contacts.

In this work, the synthesis of low-temperature oxide-type solid electrolytes by using sintering glassy  $Li_2O-B_2O_3$  additives is presented. The use of amorphous  $Li_2O-B_2O_3$ interfacial material is used to overcome the rigid nature of ceramic-oxide solid electrolytes. Inorganic  $Li_2O-B_2O_3$  interfacial material is a promising alternative to prepare all-solid-state batteries producing enough physical contacts between solid electrolyte and electrodes. This report includes results already partially published. [6,7]

#### **2.Experimental Section**

*Synthesis of materials*. The synthesis of Ta-doped LLZ by the sol-gel process was carried out following a reported procedure<sup>[8]</sup>. First, LiNO<sub>3</sub> (99%, Kanto chemicals) and La(NO<sub>3</sub>)<sub>3</sub> ·  $6 H<sub>2</sub>$ O (99.9%, Kanto chemicals) were dissolved in ethanol. Second, Ta(OC<sub>2</sub>H<sub>5</sub>)<sub>5</sub> (99.9%, High-purity chemicals),  $Zr(OC_4H_9)_4$  (85% in butanol, Wako pure chemicals) and ethyl acetoacetate (EAcAc, 99 %, Kanto chemicals) were dissolved in ethanol under argon atmosphere and stirred for 1 hour. Then, both solutions were mixed, and the resulted transparent solution was stirred at room temperature for 1 to 2 hours to obtain a sol. The obtained sol was dried under vacuum between 80 and 130℃ to obtain a dried gel that was later pulverized and heat-treated at  $700^{\circ}$  in an alumina crucible for 5 hours (1 $^{\circ}$ C min-1). Finally, 2g of this powder and 4 mL of toluene were placed in a ZrO 2 pot and grounded at  $300$  RPM for 6 hours. Then, toluene was evaporated under vacuum at  $100^{\circ}$  to obtain final LLZT calcined powder. The molar ratio of Li:La:Zr:Ta:EAcAc was  $7.15:3:1.3:0.5:1.5$  and lithium was added in 10% excess to compensate for the loss of Li during sintering. The  $Li<sub>2</sub>O B_2O_3$  sol was synthesized by the sol-gel process using trimethoxyborane (TMB, Shin-Etsu Chemicals) and lithium ethoxide (High-purity chemicals) in a molar ratio 3 : 1 and total concentration of  $40 gL-1$ . TMB was dissolved in ethanol and stabilized by addition of EAcAc under argon atmosphere. Then,  $0.1M HNO<sub>3</sub>$  was added dropwise (molar ratio TMB:HNO<sub>3</sub> of  $1:0.5$ ), and the mixture was stirred for 1 hour. In parallel, lithium ethoxide was dissolved in ethanol. Then, both solutions, TMB and lithium ethoxide, were mixed and stirred for 1 hour to obtain a precursor LBO solution. The LBO powder was synthesized by the solidstate process following a reported procedure<sup>[8,9]</sup>. Briefly, the  $Li_2O$  (Wako pure chemicals) and  $B_2O_3$  (Wako pure chemicals) in a molar ratio 3:1 were ball milled under an argon atmosphere for 40 hours under 370 RPM. Then, the milled powder was heat-treated at 210℃ for 10 hours and finally to 600°C for 5 hours to obtain  $Li_3BO_3$  powder. The  $Al_2O_3$  sol and powder were obtained by commercial source with particle size  $\sim$  50 nm and  $\sim$  1 µm, respectively. Both materials were used without any further purification or pretreatment.

*Sintering of LLZT pellets.* LBO and  $Al_2O_3$ , sols and/or powders, were added to the LLZT calcined powder and mixed in a mortar using toluene. Toluene was completely removed at 80℃ for approximately 2 hours. The calcinated LLZT powder containing sintering additives

were formed into pellets  $(\emptyset = 10 \text{mm})$  at 100 MPa (5 min) using a uniaxial press and then, were sintered at 1000°C (10h) using a heating rate of 1°C /min and intermedium step at 700 $°C$  (5h). The pellets were sintered under ambient atmosphere using alumina crucibles. The pellets were thoroughly buried in identical powder to mitigate losses of lithium and prevent any contamination with crucibles.

*Physicochemical Characterization*. Crystal phase was determined by X-ray diffraction (XRD) using a RINT 2000 Ultima RIGAKU diffractometer. Powder samples were scanned between  $10^{\circ}$  and  $60^{\circ}$  at a rate of  $2^{\circ}/\text{min}$  using Cu-Ka radiation. Morphology of the crosssection pellets were observed by scanning electron microscopy (SEM), performed on a MultiFlex 600 and JIB- 4600 F Multibeam SEM-FIB Scanning Electron Microscopes. The relative density was calculated with a geometrical dimension of the pellets and theoretical density of LLZT  $(5.11g \text{ cm-}3)$ .

*Electrochemical characterization*. HS Flat Cell HS- 3 ETK (Hohsen Corporation) was used to perform the electrochemical measurements. The conductivity of the composite solid electrolyte pellets was evaluated by the electrochemical impedance spectroscopy (EIS), under Ar atmosphere. The samples were Au-coated and sandwiched between two stainlesssteel (SS, blocking electrodes) disks used as current collectors. Symmetric cells were constructed with lithium metal heated at 175℃ . EIS measurements were conducted using an impedance analyzer (SI 1260 , Solartron) in the frequency range of 1 - 3 MHz to 100 Hz at the amplitude of 80-100mV. The impedance spectra were analyzed with ZView (Scribner Associates) to assess the ohmic total resistance (Rt), which was normalized to the pellet geometry (t: thickness and A: golden surface area) to calculate the conductivity through the usual formula  $\sigma = t/Rt.A$ .

#### **3.Results and Discussion**

The following cases were evaluated: (i) LBO and  $Al_2O_3$  in the powder states, (ii) LBO in the sol state and  $Al_2O_3$  in the powder state, and (iii) LBO and  $Al_2O_3$  in the sol states (LLZT-PP, LLZT-SP, and LLZT-SS, denoting the state of each additive (powder or sol), respectively). XRD patterns of LLZT-PP, LLZT-SP, and LLZT-SS sintered at 1000℃ confirmed the formation of expected cubic phase with the *Ia*3¯*d* space group (ICSD # 183607 ). LLZT-PP and LLZT-SP exhibited other peaks attributed to the tetragonal phase with the *I*41/*acd* space group (ICSD  $\#238686$ ), LaAlO<sub>3</sub>, and unidentified phases. The presence of the tetragonal phase is associated with the insufficient stabilization of the cubic phase, which suggests a nonuniform distribution of the sintering additives or insufficient amount of them, which could be the main reason for the promotion of secondary reactions during sintering. Nonetheless, the addition of solution-derived sintering additives leads to a single-phase cubic garnet structure with a lattice parameter in good agreement with that of LLZT  $(12.94\text{\AA})^{\{8,9\}}$ . This confirms that the liquid phase of sintering additives formed during the sintering remains almost unreactive with LLZT grains and is present in the sintered ceramic body as an amorphous phase.

Figure 1 shows cross-sectional SEM images of the LLZT pellets without and with sintering

additives, including the relative densities. The relative densities of LLZT, LLZT-PP, LLZT-SP, and LLZT-SS were 50 %, 78 %, 94 %, and 88 %, respectively. LLZT sintered in the absence of sintering additives exhibited a porous microstructure with single particles with a size of  $a$  p  $p$  r  $o$  x i m a t e  $1y$  1  $\mu$  m, indicating an insufficient densification. In contrast, the sintering additives positively contributed to the LLZT densification, where larger grains (above 20 µm) were observed as a clear signal of



Figure 1. SEM image of cross section (a) LLZT without sintering additive, (b) LLZT-SS, (c) LLZT-SP, (d) LLZT-SS

the grain growth and enhanced sintering. Notably, the relative densities of LLZT-PP and LLZT-SP were over- and under-estimated because these samples contained secondary phases as verified by XRD.

Figure 2 (top) how Nyquist plots of the electrochemical impedance of the of *LLZT-PP, LLZT-SP and LLZT-SS* pellets measured at 25℃ . The semicircles at high frequencies  $(>10 \text{ kHz})$  are associated to the resistance of the LLZT composite electrolyte involving grains and grain boundaries. The tail at low frequencies is attributed the stainless-steel blocking electrodes. The total ionic conductivity (grain + grain boundary) calculated by the fitting of impedance profiles to the equivalent circuits was 0 . 063 , 0 . 16 , and 0 . 8 mS cm−<sup>1</sup> for LLZT-PP, LLZT-SP, and LLZT-SS, respectively. Figure 2 (bottom) shows an Arrhenius plot of the LLZT



Figure 2 . (top) Impedance profiles of LLZT-PP, LLZT-SP and LLZT-SS cells using blocking Au electrode at 25℃ . (bottom) Arrhenius plot.

pellets obtained by the total ionic conductivity in the temperature range of 25– 125℃ . The activation energy was 14, 12, and 9kJ mol−<sup>1</sup> for LLZT-PP, LLZT-SP, and LLZT-SS, respectively. The lowest activation energy obtained when LLZT is sintered with LBO and  $Al_2O_3$  sols is attributed to the low resistance of the grain boundaries. In other words, the ion mobility through the grain boundaries, formed by a more uniform distribution of LBO presumably located at the grain boundaries, is facilitated by the good contact between the LLZT grains and LBO. LBO in the solid electrolyte microstructure distributes the current homogeneously and prevents dendrite nucleation and propagation, suppressing lithium dendrites up to  $10 \text{ mA cm}^{-2}$  (unpublished).

# **4.Conclusions**

The effects of  $Li_2 O-B_2 O_3$  and  $Al_2 O_3$  solution-derived sintering additives on the sinterability of LLZT solid electrolyte were studied and compared to their powder-state counterparts. The use of solution-derived sintering additives leads to a single-phase cubic garnet structure and enhanced densification. The use of in  $Li_2O-B_2O_3$  and  $Al_2O_3$  sintering of LLZT ceramic solid electrolyte achieves a high ionic conductivity of 0.8mS cm<sup>-1</sup> at 25<sup>°</sup> with low activation energy  $(9kJ \text{ mol}^{-1})$  and almost negligible contribution of the grain boundary resistance ( 10 %). The designed microstructure of the solid electrolytes plays a critical role in governing the electrochemical properties, particularly the CCD.

# **5.Acknowledgments**

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